

Mechanical behavior of double- C_{60} -end-capped poly(ethylene oxide)

T. Song, S.H. Goh*, S.Y. Lee

Department of Chemistry, National University of Singapore, 3 Science Drive, Singapore 117543, Singapore

Received 12 August 2002; received in revised form 28 November 2002; accepted 15 January 2003

Abstract

Double- C_{60} -end-capped poly(ethylene oxide) (PEO) possesses good mechanical properties arising from a network-like structure due to the aggregation of C_{60} . The tensile strength is about 20 MPa, the elongation at break exceeds 640% and the fracture toughness is more than 110 MJ/m³. The material also possesses shape recovery ability. In contrast, single- C_{60} -end-capped PEO does not possess good mechanical properties.

© 2003 Elsevier Science Ltd. All rights reserved.

Keywords: Double- C_{60} -end-capped poly(ethylene oxide); Mechanical behavior; Aggregation

1. Introduction

[60]Fullerene, C_{60} , has attracted much attention in view of its unique chemical and physical properties [1]. There are many potential applications of C_{60} -containing polymers which combine the characteristic properties of C_{60} and those of polymers such as elasticity, film formation and processability [2–5]. Recently, we reported the reinforcing effect of a functionalized C_{60} in supramolecular C_{60} -containing polymeric materials [6,7]. Ma et al. studied the mechanical properties of blends of Novolac-type phenolic resin with fullerenol polyurethane or linear polyurethane [8]. Fullerenol polyurethane offers a better improvement on the impact strength of phenolic resin (54.3%) than linear polyurethane does (27.4%).

Poly(ethylene oxide) (PEO) is widely used in pharmaceutical products, cosmetics, and food [9]. The PEOs range from low-molecular-mass liquids to hard and brittle waxes at moderate molecular mass (up to about 20,000), and to thermoplastics at high molecular mass (> ca. 100,000) [10]. The grafting of biocompatible PEO chain onto C_{60} is of special interest since the importance of fullerene in biomedical and biotechnological fields has been recognized [11–14]. Furthermore, PEO is well known not only for its remarkable biomedical and biocompatible properties but also for its simple linear structure, controlled mass, and

narrow polydispersity. Double- C_{60} -end-capped PEOs can be prepared by the reaction of azido-terminated PEO with C_{60} [15]. The cycloaddition proceeds primarily through monoaddition with little or no higher addition products, allowing C_{60} to be attached to a single PEO chain to produce C_{60} -end-capped PEOs [15–18]. In this paper, we report that when the chain ends of PEO are capped with C_{60} , the resulting material possesses good mechanical properties arising from the aggregation of C_{60} .

2. Experimental

2.1. Materials and samples

C_{60} (99.9% pure) was obtained from Peking University, China. Two PEOs were obtained from Aldrich; their number-average molecular weight (M_n)/polydispersity values are 10,000/1.06 (PEO10), and 20,000/1.08 (PEO20), respectively.

Double- C_{60} -end-capped FPEO10F and FPEO20F were prepared from PEO10 and PEO20, respectively, and characterized following the method as reported previously [15]. Basically, the hydroxyl groups of PEO were converted to chlorine groups through reaction with thionyl chloride. The chloro-terminated PEO was then reacted with sodium azide to form azido-terminated PEO which subsequently underwent cycloaddition reaction with C_{60} to afford C_{60} -end-capped PEO. Thermogravimetric analysis and X-ray

* Corresponding author. Tel.: +65-6874-2844; fax: +65-6779-1691.
E-mail address: chmgohsh@nus.edu.sg (S.H. Goh).

photoelectron spectroscopy confirm that both ends of PEO are capped with C₆₀. The end-capping of PEO by C₆₀ depresses the crystallinity by about 50%, but produces no apparent change on PEO crystallite structure [19].

The FPEOF samples for mechanical measurements, water uptake measurements and shape recovery study were prepared by solution casting from THF (1% w/v). FPEOF solutions were evaporated to dryness slowly at ambient temperature. The resulting films were then dried in vacuo at ambient temperature for 1 week.

2.2. Electron microscopy measurements

Transmission electron micrographs (TEM) were obtained with a JEOL CX100 operating at an accelerating voltage of 100 kV. For the observation of size and distribution of aggregates, a drop of dilute solution was placed onto a 200 mesh copper grid coated with carbon. The samples were dried before measurement.

Scanning electron micrographs (SEM) were obtained with a Philips XL30-FEG using an accelerating voltage of 10–20 kV. For the observation of the fracture surfaces of sample, the film was cryofractured in liquid nitrogen and the fracture surface was then sputter-coated with platinum.

2.3. Mechanical measurements

Tensile tests were made at ambient temperature on an Instron Micro Tester 5848 at a strain rate of 8.3×10^{-2} /s. The specimen dimension was 2.0 mm \times 20 mm \times 0.2 mm. Five or more specimens were tested for FPEO10F and FPEO20F, and the average values are reported.

2.4. Water uptake measurements

The sample film (20 mm \times 20 mm \times 0.2 mm) was immersed in water at room temperature. The sample was removed periodically and blotted dry with a filter paper and then weighed. The water uptake was calculated by the equation

$$\text{Water uptake (times)} = \frac{W_s - W_0}{W_0}$$

where W_0 is the original weight of the sample and W_s the weight of the water swollen sample.

Table 1
Tensile properties of FPEOFs

Polymer	Tensile strength (MPa)	Tensile modulus (MPa)	Yield strength (MPa)	Fracture toughness ^a (MJ/m ³)
FPEO10F	24.1	283	15.9	119
FPEO20F	20.1	258	16.0	110
PEO300 ^b	5.5	650	^c	~0.04

^a Fracture toughness is calculated from the total area under the stress–strain curve.

^b Source: Ref. 20.

^c For the PEO300 ($M_w = 300,000$), fracture occurs at about 1.5% strain before yielding.

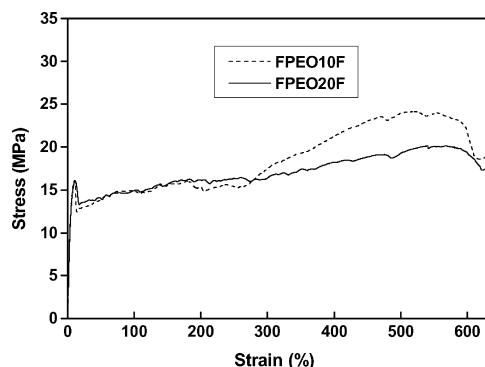


Fig. 1. Tensile stress–strain curves of FPEO10F (dash line) and FPEO20F (solid line).

3. Results and discussion

Typical stress–strain curves for the two FPEOFs are shown in Fig. 1. FPEO10F and FPEO20F develop a yield point at about 10% strain. Then, the stress drops as necking occurs and essentially stabilizes as a result of strain hardening. For FPEO10F, stress increases further above 270% strain. Both FPEOFs develop a very large (elongation > 640%) plastic deformation. Compared to their parent brittle wax-like PEO10 and PEO20, the improvement in the mechanical performance is significant. Interestingly, ductile FPEOF specimens were not broken even at 640% strain, the limit of the testing instrument. The tensile strength, tensile modulus, yield strength, and fracture toughness of FPEOFs are summarized in Table 1. For comparison, the properties of PEO300 (weight-average molecular weight = 300,000) are also shown [20]. Other than tensile modulus, the two FPEOFs are superior to PEO300, especially the fracture toughness. As compared to PEO300, the ultimate strain of FPEOF is at least 427 times higher and the toughness of FPEOF is at least 2700 times better. The tensile modulus of FPEOF is lower than that of PEO300, demonstrating that the C₆₀-containing PEOs are relatively ductile PEO materials. Fig. 2 shows the photographs of FPEOF specimens before and after deformation.

Thermoplastic elastomers based on PEO/PBT (polybutylene terephthalate) multiblock copolymers are built up of hard segments (PBT) and soft segments (PEO) [21]. The tensile strength varies from 8 to 23 MPa, elongation at break from 500 to 1300%, and water uptake from 4 to 210%. Apparently, the mechanical properties of FPEOF are as

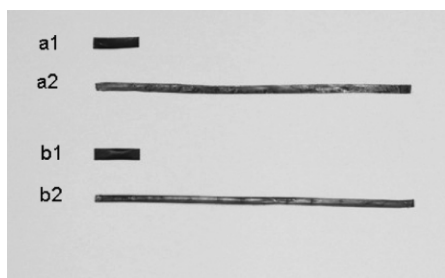


Fig. 2. FPEO10F specimen before (a1) and after (a2) deformation; FPEO20F specimen before (b1) and after (b2) deformation.

good as, if not better than, those of PEO/PBT thermoplastic elastomers.

C_{60} -containing polymers and C_{60} derivatives form aggregates in solution or in solid state [22–26]. In principle, double- C_{60} -end-capped polymers can aggregate to form a network-like structure. The aggregation of FPEO10F and FPEO20F was demonstrated by TEM using dried sample obtained from the THF solutions (Fig. 3). Fig. 4 shows the SEM micrographs of fracture surfaces of FPEO10F and FPEO20F samples. Spherical C_{60} aggregates in the order of tens of nanometers are observed. The aggregates serve as crosslinks, similar to those of the polystyrene domains in polystyrene-*block*-polybutadiene-*block*-polystyrene (S-B-S) thermoplastic elastomers [27] (Scheme 1). Another evidence for the aggregation of FPEOF is that the cast films of FPEOF cannot be re-dissolved in water but they only swell to a great extent and this will be discussed later. However, the films can be re-dissolved in hot chlorobenzene under sonication for several hours. This may be ascribed to the fact that water is a poor solvent for C_{60} so that it cannot disrupt the aggregates but chlorobenzene is a good solvent for C_{60} and PEO to facilitate the dissolution. Similarly, C_{60} -end-capped three-arm PEO can also be re-dissolved in chlorobenzene [28]. Therefore, the crosslinks originated from amphiphilic FPEOF aggregation are physical rather than chemical. This also affirms the ‘S-B-S’ model for the FPEOF materials. To further confirm the validity of the model, single- C_{60} -end-capped PEO (FPEO) was also synthesized by cycloaddition reaction of monoazido-terminated PEO with C_{60} [18]. The resulting FPEO is brittle, wax-like powder just like its parent poly(ethylene glycol) monomethyl ether (MPEO) (M_n /polydispersity is 2200/1.07). Although FPEO also aggregates in THF solution as observed by TEM (Fig. 3), it does not show any improvement in mechanical properties over its parent MPEO. Aggregates originated from single- C_{60} -end-capped FPEO chains do not interconnect to form a network. This further confirms that only double- C_{60} -end-capped PEO (FPEOF) can form a network-like structure to achieve high performance. Similarly, only triblock S-B-S but not diblock S-B is a useful thermoplastic elastomer.

Fig. 5 shows that FPEOF films become fully swollen in water in about 1 min. The water uptake is about seven times for FPEO10F and about nine times for FPEO20F. The lower

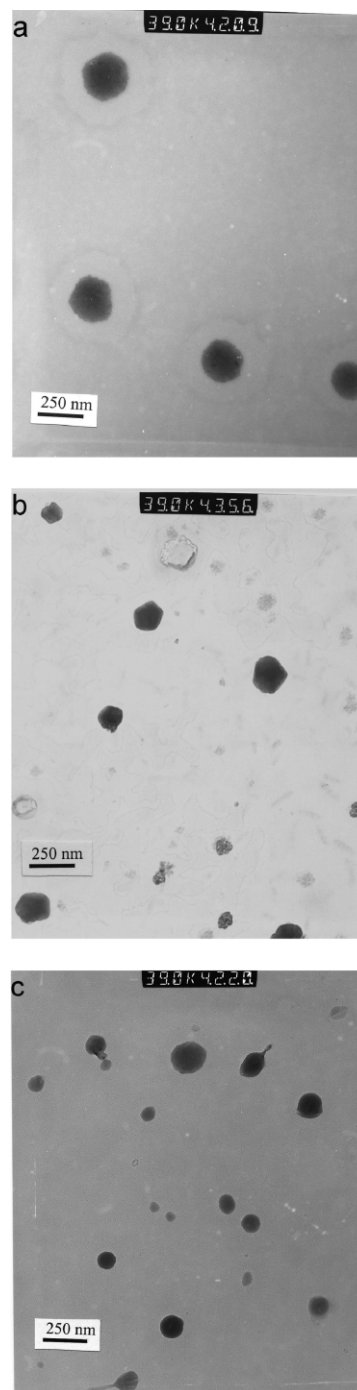
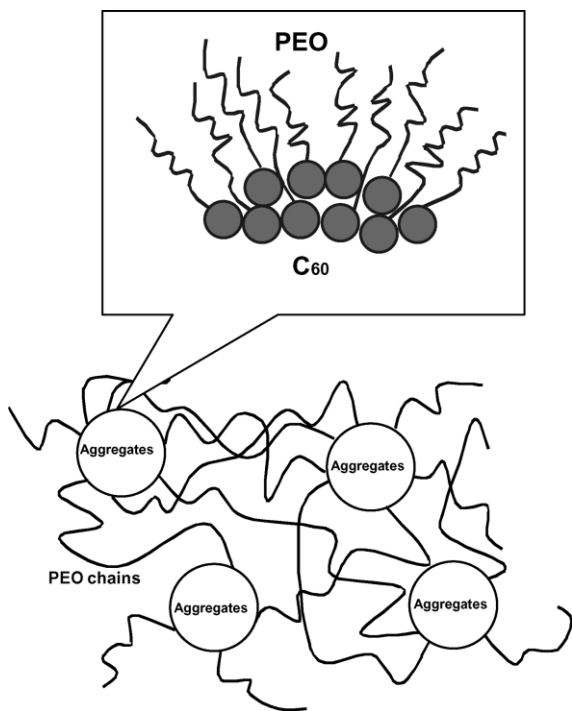
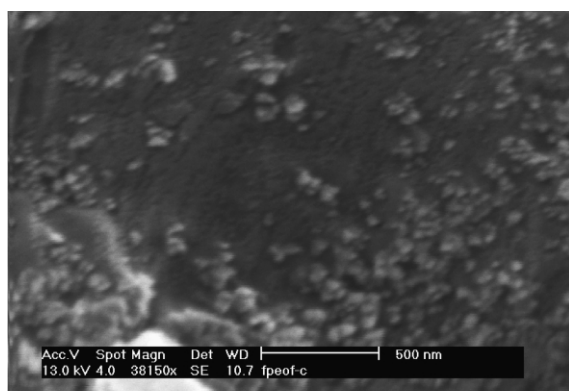


Fig. 3. TEM of aggregates prepared from the THF solutions for (a) FPEO, (b) FPEO10F, and (c) FPEO20F.

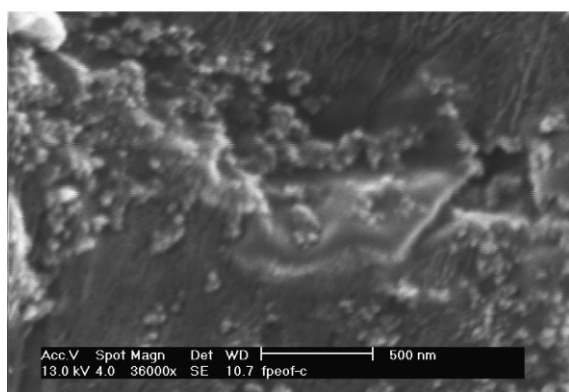
extent of swelling of FPEO10F than that of FPEO20F is consistent with the fact that a highly crosslinked material swells to a lesser extent as compared to a lightly crosslinked material. Furthermore, the swollen FPEOF films show shape recovery ability. The swollen films recover completely to their original shapes and sizes without loss in mechanical performance after being dried at 55 °C for 1 h. Fig. 6 demonstrates the swelling and recovering process of FPEO10F. Irregularly drawn FPEOF films recover



Scheme 1. Schematic diagram of FPEOF.



(a)



(b)

Fig. 4. SEM of fracture surfaces of (a) FPEO10F and (b) FPEO20F.

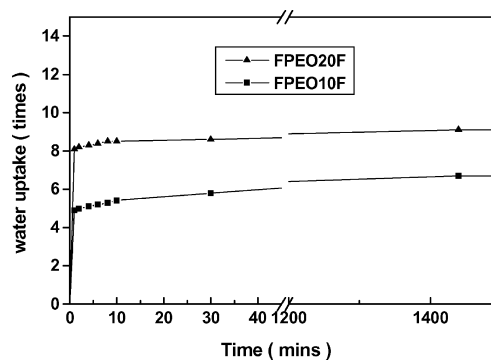


Fig. 5. Water uptake curves for FPEOFs at room temperature.

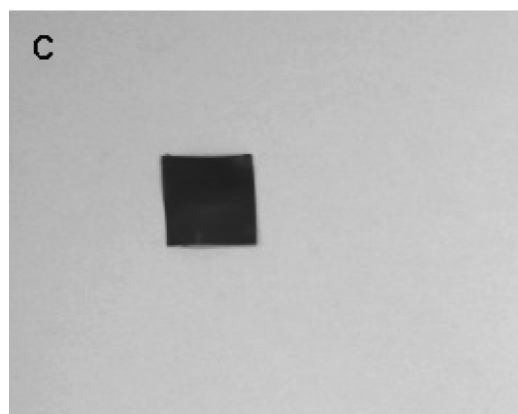
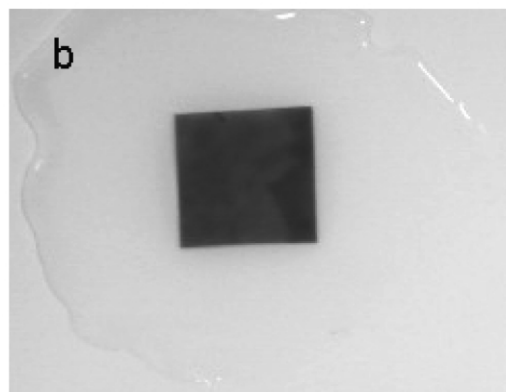
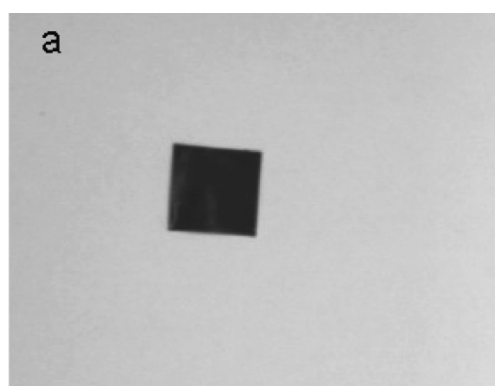


Fig. 6. Photographs for (a) the original FPEO10F film, (b) the water-swollen FPEO10F film, and (c) the recovered FPEO10F film after being dried.

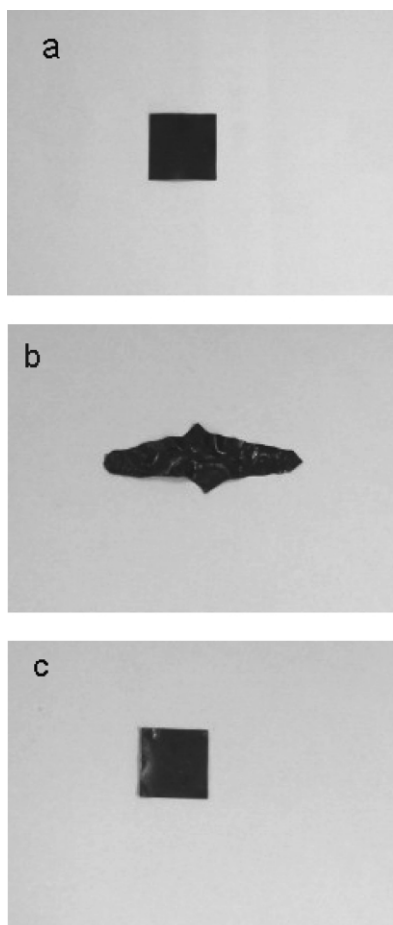


Fig. 7. Photographs for (a) the original FPEO10F film, (b) the irregularly drawn FPEO10F film, and (c) the recovered FPEO10F film after being heated.

completely to their original shapes and sizes after being heated at 55 °C for about 10 min (Fig. 7).

4. Conclusions

The two double- C_{60} -end-capped PEOs possess good mechanical properties. For example, the fracture toughness is 2700 times more than that of PEO300. FPEOFs can sustain a very large (elongation >640%) plastic deformation prior to fracture. The good mechanical behavior of FPEOFs arises from the aggregation of C_{60} moieties to form a network-like structure. It is envisaged that other double- C_{60} -end-capped polymers may also possess good mechanical properties. The mechanical properties of thermoplastic elastomers based on ‘S-B-S’ type or multiblock hard/soft segmental copolymers deteriorate when the hard domains soften at high temperatures. Although we were unable to

conduct tensile tests at high temperatures, we envisage that the mechanical properties of the two FPEOF samples are not likely to deteriorate significantly, at least at moderately high temperatures, since C_{60} molecules are not softened. Furthermore, in view of the biomedical and biotechnological properties of C_{60} and PEO, such double- C_{60} -end-capped PEO may find possible biomedical/biotechnological applications.

References

- [1] For recent reviews on fullerene chemistry see: Prato M. *J Mater Chem* 1997;7:1097. Karaulova EN, Bagrii EI. *Russ Chem Rev* 1999;68:889. Diederich F, Gomez-Lopez M. *Chem Soc Rev* 1999;28:263.
- [2] Dai L, Mau AWH. *Adv Mater* 2001;13:899.
- [3] Geckeler KE, Samal S. *Polym Int* 1999;48:743.
- [4] Dai L. *J Macromol Sci—Rev Macromol Chem Phys* 1999;C39:273. Dai L. *Polym Adv Technol* 1999;10:357.
- [5] Eklund PC, Rao AM. *Fullerene polymers and fullerene polymer composites*. Berlin: Springer; 2000.
- [6] Ouyang JY, Goh SH, Li Y. *Chem Phys Lett* 2001;347:344.
- [7] Ouyang JY, Goh SH. *Fullerenes Nanotubes Carbon Nanostruct* 2002; 10:183.
- [8] Ma CCM, Sung SC, Wang FY, Chiang LY, Wang LY, Chiang CL. *J Polym Sci, Part B: Polym Phys* 2001;39:2436.
- [9] Harris JM, Zalipsky S. *Poly(ethylene glycol)—chemistry and biological applications*. Washington, DC: American Chemical Society; 1997.
- [10] Wilks ES. *Industrial polymers handbook—products, processes, applications*. Weinheim: Wiley-VCH; 2001.
- [11] Friedman SH, DeCamp DL, Sijbesma RP, Srdanov G, Wudl F, Kenyon GL. *J Am Chem Soc* 1993;115:6506.
- [12] Jensen AW, Wilson SR, Schuster DI. *Bioorg Med Chem* 1996;4:767.
- [13] Da Ros T, Prato M. *Chem Commun* 1999;663.
- [14] Tabata Y, Ikada Y. *Pure Appl Chem* 1999;71:2047.
- [15] Huang XD, Goh SH. *Macromolecules* 2000;33:8894.
- [16] Hawker CJ, Saville PM, White JW. *J Org Chem* 1994;59:3503.
- [17] Delpeux S, Beguin F, Benoit R, Erre R, Manolova N, Rashkov I. *Eur Polym J* 1998;34:905.
- [18] Huang XD, Goh SH, Lee SY. *Macromol Chem Phys* 2000;201:2660.
- [19] Huang XD, Goh SH. *Macromolecules* 2001;34:3302.
- [20] Tsou L, Sauer JA, Hara M. *J Polym Sci Part B: Polym Phys* 2000;38: 1377.
- [21] Deschamps AA, Grijpma DW, Feijen J. *Polymer* 2001;42:9335.
- [22] Okamura H, Ide N, Minoda M, Komatsu K, Fukuda T. *Macromolecules* 1998;31:1859.
- [23] Wang XH, Goh SH, Lu ZH, Lee SY, Wu C. *Macromolecules* 1999;32: 2786.
- [24] Zhou SQ, Burger C, Chu B, Sawamura M, Nagahama N, Toganoh M, Hackeler UE, Isobe H, Nakamura E. *Science* 2001;291:1944.
- [25] Ederlé Y, Mathis C. *Fullerene Sci Technol* 1996;4:1177.
- [26] Okamura H, Minoda M, Fukuda T, Miyamoto T, Komatsu K. *Macromol Rapid Commun* 1999;20:37.
- [27] Holden G, Legge RN, Quirk RP, Schroeder HE. *Thermoplastic elastomers*. New York: Carl Hanser; 1996.
- [28] Taton D, Angot S, Gnanou Y, Wolert E, Setz S, Duran R. *Macromolecules* 1998;31:6030.